OLTAGE

(HVPS) Condatas AG

RAIL TO RAIL OPERATIONAL AMPLIFIER

## **KEY FEATURES**

- LOW COST
- RAIL TO RAIL INPUT & OUTPUT
- WIDE SUPPLY RANGE  $\pm 5V \pm 50V$
- SINGLE SUPPLY OPERATION
- HIGH OUTPUT CURRENT 50A
- 600 WATT OUTPUT CAPABILITY
- 300 WATT DISSIPATION CAPABILITY
- INTEGRATED HEAT SINK AND FAN
- TEMPERATURE REPORTING
- OVER-TEMP SHUTDOWN

## **APPLICATIONS**

- LINEAR MOTOR DRIVE
- INDUSTRIAL AUDIO
- SEMICONDUCTOR TESTING
- VIBRATION CANCELLATION
- PROGRAMMABLE POWER SUPPLY

## **DESCRIPTION**

The PAD147 rail to rail power operational amplifier is constructed with surface mount components to provide a cost effective solution for many industrial applications where it is important to obtain a maximum output signal with limited supply voltages. The PAD147 out-performs much more expensive hybrid or rack-mount amplifiers in a footprint only 90mm square. User selectable external compensation tailors the amplifier's response to the application requirements. Fourwire programmable current limit is built-in. The PAD147 also features a substrate temperature reporting analog output and over-temp shutdown. The amplifier circuitry is built on an insulated metal substrate mounted to an integral heat sink and fan assembly. No BeO is used in the PAD147. The resulting module is a small, high performance turn-key solution for many industrial applications. For custom installations the PAD147-1 is available without the heat sink and fan

PAD147 mounted in evaluation kit

# **A NEW CONCEPT**

A critical task in any power amplifier application is cooling the amplifier. Until now component amplifier manufacturers often treated this task as an after-thought, left for the user to figure out. At **Power Amp Design** the best heat sink and fan combination is chosen at the start and becomes an integral part of the overall amplifier design. The result is the most compact and volumetric efficient design combination at the lowest cost. In addition, this integrated solution concept offers an achievable real-world power dissipation rating, not the ideal rating usually cited when the amplifier case is somehow kept at 25°C. The user no longer needs to specify, procure or assemble separate components.

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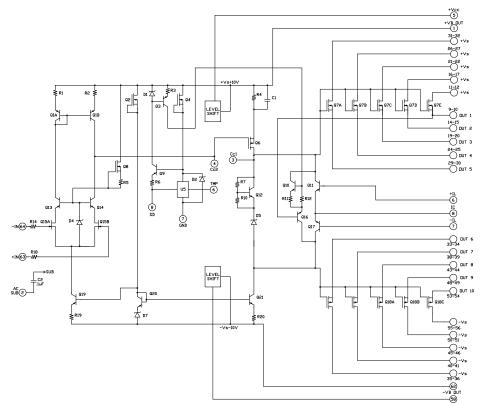
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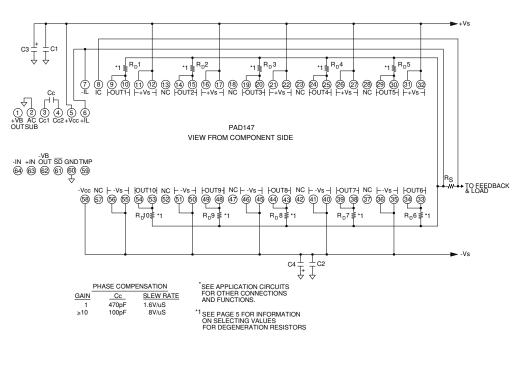
# PAD147 Rev A



### EQUIVALENT CIRCUIT



## **AMPLIFIER PINOUT & CONNECTIONS**









#### ABSOLUTE MAXIMUM RATINGS SPECIFICATIONS

	ABSOLUTE MAXIM	UM RATIN	GS				
SUPPLY VOLTAGE, +Vs to -Vs 1					+Vs to	-Vs	
POWER DISSIPATION, internal, DC 3		TEMPERATURE, pin solder, 10s			300°C		
		TEMPERATURE RANGE, storage				$-40$ to $70^{\circ}C^{5}$	
OPERATING TEMPERATURE, heat sin		TEMPERATURE RANGE, storage, PAD147-1 105°C					
		1					
PARAMETER	TEST CONDITIONS <sup>1</sup>	MIN	ТҮР	MAX	PAD147-1 <sup>7</sup>	UNITS	
			1	5		N	
OFFSET VOLTAGE			1	5		mV	
OFFSET VOLTAGE vs. temperature	Full temperature range		20	50		µV/ <sup>o</sup> C	
OFFSET VOLTAGE vs. supply				20		μV/V	
BIAS CURRENT, initial <sup>3</sup>				100		pA	
BIAS CURRENT vs. supply				0.1		pA/V	
OFFSET CURRENT, initial				50		pA	
INPUT RESISTANCE, DC			100			GΩ	
INPUT CAPACITANCE			4			pF	
COMMON MODE VOLTAGE RANGE		± Vs				V	
COMMON MODE REJECTION, DC		92				dB	
NOISE, referred to input	100kHz bandwidth, 1k $\Omega$ R <sub>s</sub>		1			mVrms	
GAIN							
OPEN LOOP	$R_{L}=100\Omega, C_{C}=100pF$	100				dB	
GAIN BANDWIDTH PRODUCT @ 1MHz			1			MHz	
PHASE MARGIN	Full temperature range	60				degree	
OUTPUT							
VOLTAGE SWING	$I_{O} = 50A$			+Vs-1		V	
VOLTAGE SWING	$I_0 = -50A$			-Vs+1.5		V	
CURRENT, continuous, DC	10 5011	30		1311.5		A	
SLEW RATE, $A_V = -10$	$C_{c} = 100 pF$	6.4	8			V/µS	
SETTLING TIME, to 0.1%	2V Step	0.1	2			μS	
RESISTANCE	No load, DC		2			Ω	
	No load, DC		2			52	
SHUTDOWN			1			0	
TRANSITION TIME, off	$\pm$ output voltage to zero		1			μS	
TRANSITION TIME, on	Zero to normal output		2			μS	
CURRENT	internal currents dumped into load		± 6			mA	
POWER SUPPLY							
VOLTAGE <sup>7</sup>		± 5	± 35	± 50		V	
CURRENT, quiescent			80	88		mA	
+VB OUT, -VB OUT, load	Output voltage for accessory module	e		± 1.5		mA	
THERMAL							
RESISTANCE, AC, junction to air or case <sup>4</sup>	Full temperature range, $f \ge 60$ Hz			0.28 to air	0.13 to case	<sup>o</sup> C/W	
RESISTANCE, DC, junction to air	Full temperature range			0.41 to air	0.2 to case	°C/W	
TEMPERATURE RANGE, substrate		-40		105		°C	
TEMPERATURE RANGE, ambient		-40		70	105	°C	
TEMPERATURE, shutdown, substrate			110			°C	
FAN, 92mm dc brushless, ball bearing							
OPERATING VOLTAGE			12		NA	V	
OPERATING CURRENT			290		NA	mA	
AIR FLOW			50		NA	CFM	
RPM			2800		NA	RPM	
NOISE			33		NA	dB	
L10, life expectancy, 70 <sup>o</sup> C <sup>6</sup>			45		NA	kHrs	
L10, life expectancy, $40^{\circ}C^{6}$			60		NA	kHrs	
L10, life expectancy, 40°C°			00		INA	KIIIS	

NOTES

1. Unless otherwise noted:  $T_c=25^{\circ}C$ , compensation Cc=470pF, DC input specifications are  $\pm$  value given, power supply voltage is typical rating.

2. Derate internal power dissipation to achieve high MTBF.

3. Doubles for every 10<sup>o</sup>C of case temperature increase.

4. Rating applies if the output current alternates between both output transistors at a rate faster than 60Hz.

5. Limited by fan characteristics. During operation, even though the heat sink may be at 85°C or more the fan will be at a lower temperature.

6. L10 refers to the time it takes for 10% of a population of fans to fail. Lower ambient temperature increase fan life.

7. Specifications for the PAD147-1 are the same as for the PAD147 except as shown in this column.





#### **COMMON MODE RANGE**

The PAD147 is a rail to rail operational amplifier. This means that it works equally well with the input pins biased to either supply rail or at any voltage in between. The most common application utilizing this function is the single supply voltage amplifier where the +IN pin and the –Vs supply pin are grounded.

#### **OUTPUT SWING**

With no load the output voltage of the PAD147 can swing to either supply voltage rail. As the load current increases the maximum output swing is reduced, but at 50A output the swing from the positive supply rail is less than 1V and less than 1.5V from the negative supply rail. This does not include any voltage drop due to the sensing voltage required for the current limit circuit to operate or voltage drop across the degeneration resistors (see page 5).

#### **CURRENT LIMIT**

The current limiting function of the PAD147 is a versatile circuit that can be used to implement a four-wire current limit configuration or, in combination with some external components can be configured to implement a fold-over current limit circuit. The four-wire current limit configuration insures that parasitic resistance in the output line, Rp, does not affect the programmed current limit setting. See Figure 1. The sense voltage for current limit is 0.65V. Thus:

$$I_L = \frac{0.65V}{R_s}$$

Where  $I_L$  is the value of the limited current and  $R_S$  is the value of the current limit sense resistor.

In addition, the sense voltage has a temperature coefficient approximately equal to  $-2.2 \text{mV}/^{\circ}\text{C}$ . The fold-over function reduces the available current as the voltage across the output transistors increases to help insure that the SOA of the output transistors is not exceeded. Refer to **Application Circuits** for details on how to connect the current limit circuitry to implement either a four-wire current limit or current limit with a fold-over function.

In some applications better current limiting protection and a lower sense voltage may be desired. In this case the PAD147 can be operated with the PAD125 Current Limit Accessory Module. See Figure 3 in the applications section and the PAD125 data sheet for more details.

#### **COOLING FAN**

The PAD147 relies on its fan for proper cooling of the amplifier. Make sure that air flow to the fan and away from the

heat sink remains unobstructed. To eliminate electrical noise created by the cooling fan we recommend a  $47\mu$ F capacitor placed directly at the point where the fan wires connect to the PCB. See application note AN-24 for further details.

#### **MOUNTING THE AMPLIFIER**

The amplifier is supplied with four 4-40 M/F hex spacers at the four corners of the amplifier. Since the male threaded ends of the spacers extend beyond the amplifier pins the spacers provide a convenient alignment tool to guide the insertion of the amplifier pins into the circuit board. Once the amplifier is seated secure the module with the provided 4-40 nuts and torque to 4.7 in lb [53 N cm] max. See "**Dimensional Information**" for a detailed drawing. It is recommended that the heat sink be grounded to the system ground. This can easily be done by providing a grounded circuit board pad around any of the holes for the mounting studs.

#### **TEMPERATURE REPORTING**

An analog output voltage is provided (pin 59, TMP) relative to ground and proportional to the temperature in degrees C. The slope is approximately -10.82mV/°C. The output voltage follows the equation:

$$T = (2.127 - V) (92.42)$$

Where V is the TMP output voltage and T is the substrate temperature in degrees C.

#### **THERMAL SHUTDOWN**

The temperature monitoring circuit automatically turns off the output transistors when the substrate temperature reaches 110°C. When the substrate cools down 10°C the output is enabled once again. The thermal shutdown feature is activated either by amplifier overloads or a failure of the fan circuit.

#### **EXTERNAL SHUTDOWN**

When pin 61 ( $\overline{SD}$ ) is taken low (ground) the output stage is turned "off" and remains "off" as long as pin 61 is low. When pin 61 is monitored with a high impedance circuit it also functions as a flag, reporting when the amplifier is shut down. A "high" (+5V) on pin 61 indicates the temperature is in the normal range. A "low" (ground) indicates a shutdown condition. See **Application Circuits** for details on how to implement an external shutdown circuit and how to monitor the shutdown status.





## OPERATING CONSIDERATIONS CONTINUED

#### PHASE COMPENSATION

The PAD147 **must** be phase compensated to operate correctly. The compensation capacitor,  $C_c$ , is connected between pins 4 and 5. On page 7, Typical Performance Graphs, you will find plots for small signal response and phase response using compensation values of 100pF and 470pF. The compensation capacitor must be an NPO type capacitor rated for the full supply voltage (100V). On page 2, under Amplifier Pinout and Connections, a table gives recommended compensation capacitance values for various gains and the resulting slew rate for each capacitor value.

#### **DEGENERATION RESISTORS**

The PAD147 derives its high power dissipation rating from the use of parallel output MOSFET transistors. To insure that the load current is distributed equally between the output transistors ten external source degeneration resistors are needed. See  $R_D1-R_D10$  in the external connections diagram on page 2. The value of the resistors changes depending on the total supply voltage needed for the application. The SOA power dissipation of the amplifier (300 watts dc) determines the maximum load current that the amplifier can supply with the needed total supply voltage. *To insure that the amplifier is not damaged the correct value of degeneration resistors is critical. Do not operate the amplifier without the proper value of degeneration resistors.* 

All of the ten degeneration resistors will be the same value and can be calculated by:

$$R_D = \frac{0.75V_T}{225} - 0.035\Omega$$

Where  $R_D$  is the value of each degeneration resistor and  $V_T$  is the total power supply voltage from +Vs to -Vs.

The following table shows calculated degeneration resistor values  $(\mathbf{R}_D)$  for various total supply voltages  $(\mathbf{V}_T)$ . Column (**O**) shows standard values that can be used from the Vishay/Dale resistor lines RS02B and LVR. These are also the resistor values supplied in the EVAL147 evaluation kit for the PAD147.

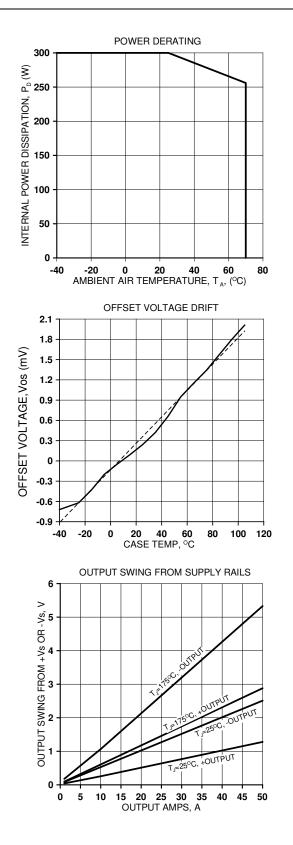
VT	R <sub>D</sub>	0	Watt
100	0.298	0.30	3
90	0.265	0.25	3
80	0.231	0.25	3
70	0.198	0.20	3
60	0.165	0.15	3
50	0.131	0.15	3
40	0.098	0.10	3
30	0.065	0.05	5
20	0.031	0.03	5
10	0.00	0.00	-

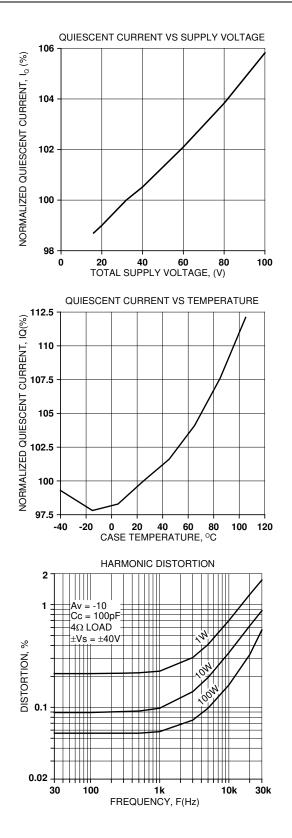
Resistors are to be 3 or 5 watt as shown in the table, 1% tolerance and preferably non-inductive, as inductive resistors may cause the output stage to oscillate. The resistors available from Power Amp Design are of the inductive wire-wound type but have been found to be adequate for this application. These resistors are also available with non-inductive windings but are not usually stocked by distributors. The use of thick film chip resistors is not recommended. Thick film, metal film or powdered metal resistors types are suitable but may be either expensive or unavailable in the required values.





# PAD147 TYPICAL PERFORMANCE GRAPHS

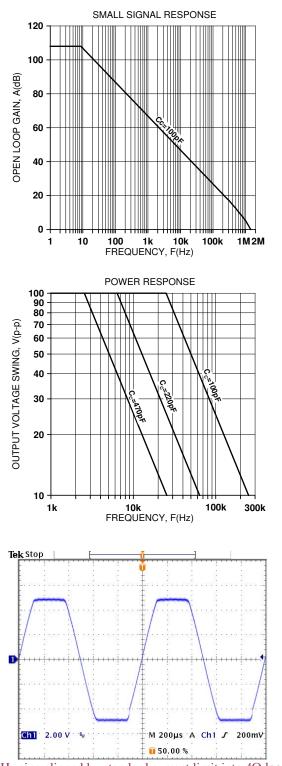




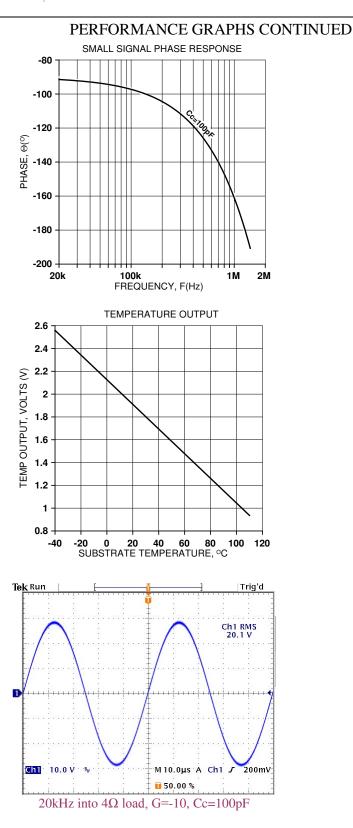




# **PAD147**



#### 1kHz sine clipped by standard current limit into $4\Omega$ load

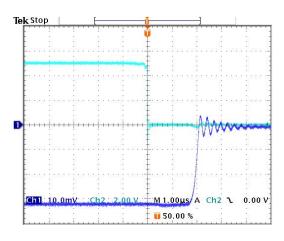






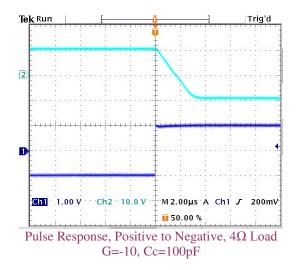


# **PAD147**



## SHUTDOWN RESPONSE, POSITIVE OUTPUT TO ZERO TRANSITION

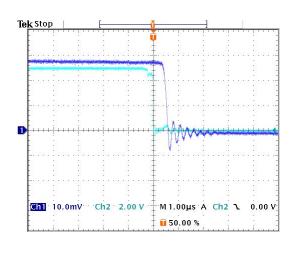
The oscilloscope display at the right shows an expanded view of a 1kHz 1.2A p-p amplifier output signal being interrupted near the positive peak by a shutdown signal on Ch2. The Ch1 display shows the output *current* going to zero about  $0.5\mu$ S after the shutdown signal goes low. The ringing in the output signal is due to inductance in the output line.

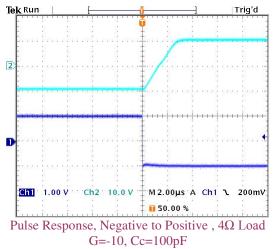


# PERFORMANCE GRAPHS CONTINUED

# SHUTDOWN RESPONSE, NEGATIVE OUTPUT TO ZERO TRANSITION

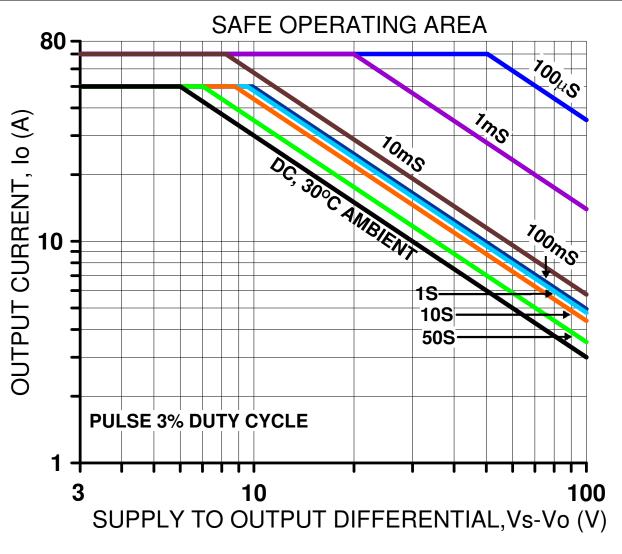
The oscilloscope display at the left shows an expanded view of a 1kHz 1.2A p-p amplifier output signal being interrupted near the negative peak by a shutdown signal on Ch2. The Ch1 display shows the output *current* going to zero about  $2\mu$ S after the shutdown signal goes low. The ringing in the output signal is due to inductance in the output line.











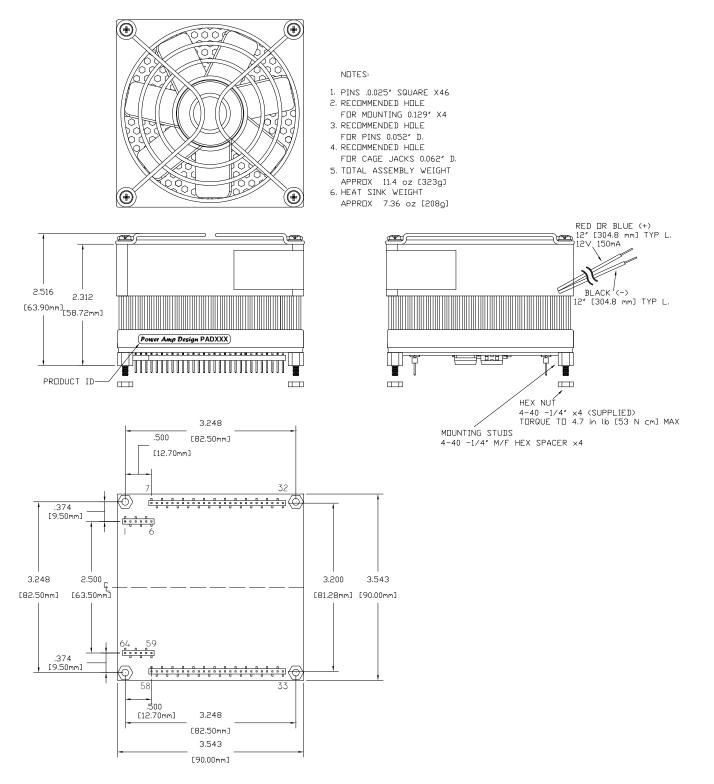
# SAFE OPERATING AREA

The safe operating area (SOA) of a power amplifier is its single most important specification. The SOA graph presented above serves as a first approximation to help you decide if the PAD147 will meet the demands of your application. But a more accurate determination can be reached by making use of the **PAD Power**<sup>TM</sup> spreadsheet which can be found in the **Power Amp Design** website. While the graph above adequately shows DC SOA and some pulse information it does not take into account ambient temperatures higher than 30°C, AC sine, phase or non-symmetric conditions that often appear in real-world applications. The **PAD Power**<sup>TM</sup> spreadsheet takes all of these effects into account.



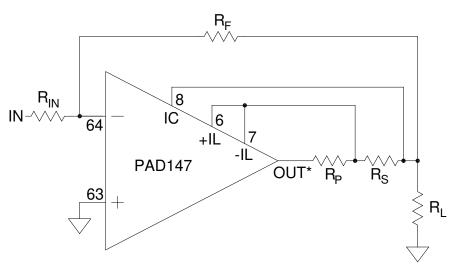


# PAD147 DIMENSIONAL INFORMATION



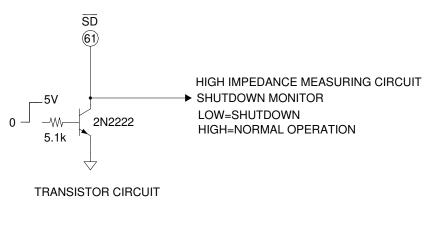


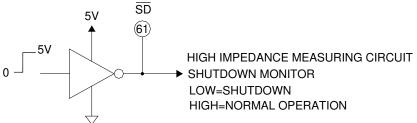




\*9-10,14-15,19-20,24-25,29-30,33-34,38-39,43-44,48-49,53-54

FIGURE 1. 4-WIRE CURRENT LIMIT





OPEN COLLECTOR OR OPEN DRAIN LOGIC GATES CIRCUIT

## FIGURE 2. EXTERNAL SHUTDOWN WITH MONITOR







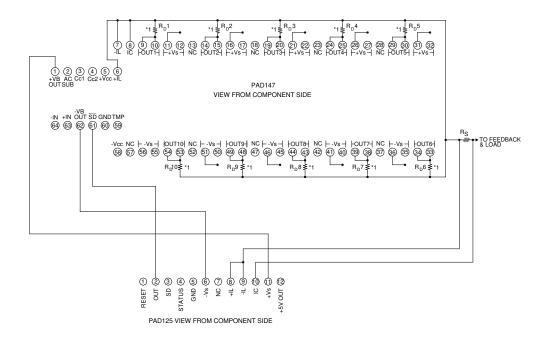
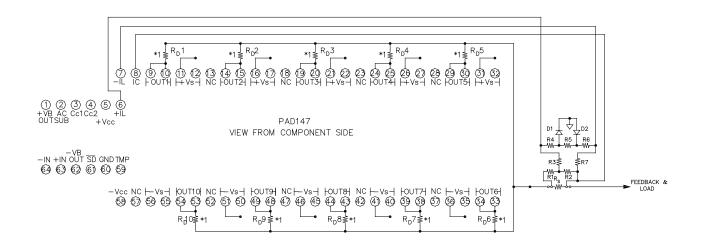


FIGURE 3 USING THE PAD147 WITH THE PAD125







With the three current limit function pins (pins 37-39) dual slope current limiting can be implemented that more closely approximates the SOA curve of the amplifier than can be achieved with standard current limiting techniques. Values for resistors R1-R7 and R<sub>s</sub> can be calculated using the **PAD Power**<sup>TM</sup> spreadsheet that can be downloaded from the Power Amp Design web site.

